DESIGN CALCULATION AND DRAWING FOR LONGITUDINAL GUIDED BEARING

(Ch. 516+938)

PROJECT: FOUR LANING OF JHANJHI TO DEMOW SECTION OF NH-37 FROM EXISTING CH. K 491+050 TO KM 535+250 (DESIGN CH. KM 4900+800 TO KM 534+800) IN THE STATE OF ASSAM UNDER EPC MOD

CLIENT: *NATIONAL HIGHWAYS & INFRASTRUCTURE DEVELOPMENT CORPORATION LTD. (NHIDCL)*

CONTRACTOR : *M/S KAMAC-SHIVA HARLALKA (JV)*

MANUFACTURER:

M/S KARMA ENTERPRISE, GUWAHATI,ASSAM

Design Calculation of SLS- 1647 KN, ULS- 2365 KN Longitudinal Guided Bearing

TYPE OF BEARING : **LG** **TYPE: B3** **Conc. Grade for Pedestal M 45**
REVISION : **00** **CH: 516+938** **Conc. Grade for Superstructure M 50**

DESIGN DATA FOR BEARING DESIGN (LOADS)

LOADING PARAMETERS	SLS		ULS	
UNITS	MT	kN	MT	kN
VERTICAL MAXIMUM LOAD	167.94	1647.00	241.16	2365.00
VERTICAL MINIMUM LOAD	68.63	673.00	117.27	1150.00
VERTICAL PERMANENT LOAD	85.96	843.00		
HORIZONTAL LOADS				
ACTING IN LONGITUDINAL DIRECTION	0.00	0.00	0.00	0.00
ACTING IN TRANSVERSE DIRECTION	0.00	0.00	0.00	0.00
RESULTANT HORIZONTAL LOADS		0.00		0.00
DISPLACEMENT				
LONGITUDINAL (MM)	+ 21.00	-21.00	42.00	
TRANSVERSE (MM)	0.00	0.00	0.00	
ROTATION (RADIAN)	0.0038	+ 0	=	0.004

Assume Permanent Rotation	q p	=	0.41	x	0.004	=	0.002
Assume Varriable Rotation	q v	=	0.59	x	0.004	=	0.002

MATERIALS

Steel Stress (Working) for Design Use 340 MPa (Grade-340-570W) AS PER IS - 1030
HT Bolts shall conform to Grade 8.8 of IS : 1364
Elastomer shall be of hardness 50 + / - 5 conforming to IRC : 83 (Part III) - 2018 Table - 4.3

DIMENSION DETAILS OF BEARING COMPONENTS

ELASTOMERIC PAD			
PAD DIAMETER	=	di	325 mm
PAD TICKNESS	=	he	24 *mm*
PTFE			
PTFE DIAMETER	=	Dptfe	325 mm
PTFE THICKNESS	=	Tptfe	5 mm
CYLINDER			
CYLINDER CONCRETE CONTACT DIAMETER	=	Do	395 mm
CYLINDER BASE THICKNESS	=	kb	20 mm
CYLINDER INNER DIAMETER	=	Di = di	325 mm
CYLINDER OUTER DIAMETER	=	do	375 mm
HEIGHT OF CYLINDER	=	hc	36 mm
WALL THICKNESS	=	Tcw	25.0 mm
INTERMEDIATE COMPONENT	=		
LENGTH	=	Lic	365 mm
WIDTH	=	Wic	365 mm
INTERMEDIATE COMPONENT ABOVE THICKNESS	=	**Tp**	12 mm
INTERMEDIATE COMPONENT PROJECTION	=	**hp**	22 mm
VERTICAL FACE	=	**w**	6 mm
TOP PLATE			
EFFECTIVE CONCRETE CONTACT DIAMETER	=	**Dtpeff**	375 mm
LENGTH	=	Lt	420 mm
WIDTH	=	Bt	410 mm
THICKNESS	=	Tt	22 mm
S/S SHEET LENGTH	=	Lss	410 mm
S/S SHEET WIDTH	=	Bss	370 mm
S/S SHEET THICKNESS	=	Tss	3 mm
GUIDE BAR LENGTH	=	Lgb	420 mm
GUIDE BAR WIDTH	=	ku	15 mm
GUIDE BAR HEIGHT	=	Hgb	18 mm

Design Calculation of SLS- 1647 KN, ULS- 2365 KN Longitudinal Guided Bearing

ANCHORAGE

BOLTS DIAMETER	=	Dbolt	16 mm
BOLTS LENGTH	=	Lbolt	35 mm
BOLTS PER COMPONENT	=	Nbolt	4 NOS.
GRADE OF BOLTS	=	GR.bolt	8.8
ANCHORAGE COLLOR LENGTH	=	CL	56 mm
ANCHORAGE COLLOR THICKNESS	=	C thk	12 mm
SLEEVE LENGTH (Superstructure)	=	Ls	110 mm
SLEEVE DIAMETER (Superstructure)	=	Ds	40 mm
SLEEVE LENGTH (Pedestal)	=	Lp	120 mm
SLEEVE DIAMETER (Pedestal)	=	Dp	40 mm

GENERAL

NO. OF BRASS SEALING RINGS	=	Nbr	2 NOS.
TOTAL THICKNESS OF RINGS	=	Tbr	4.0 mm
GAP BETWEEN CYLINDER & TOP COMPONENT	=	h4	10 mm

TOTAL BEARING ASSEMBLY HEIGHT = HT 105.2 mm

Calculation for Permissible Stresses in Pedestal Concrete

Bottom

Cylinder Concerte Contact Diameter = 395 mm

Loaded area (Aco p x Do ^ 2/4) = 122541.75 mm^2

Required Pedestal Size for Dispersion = 790.00 x 790 mm

Dispersed area ($A_{c1 = p x d ^ 2/4}$) = 490167 mm^2

Top

Top Component Contact Diameter = 375 mm

Loaded area (A_2 = p x Dtpeff ^ 2/4) = 110446.62 mm^2

Required Superstructure Size for Dispersion = 750.00 x 750 mm

Dispersed area ($Ac_{1 - p x d ^ 2/4}$) = 441786.47 mm^2

DESIGN CALCULATIONS :-
REF. CODE : IRC:83 (Part-III)-2018

Design of Pad (Clause - 5.2.3.2)

Effective diameter of Pad	Dpad		325	mm
Area of pad = p x d ^ 2/4	a		82991.0714	mm²
Vertical Load	Nsd	2365.00		kN
Direct Pressure Nsd / a	pa	28.50		N/mm²
(Nsd / a) x Ym		37.05		N/mm²
fe,k		60.00		N/mm²
		OK		

Check Compression at edge of Neoprene Pad (Clause - 5.2.3.4)

Max. Permitted = 15 % of he	3.60		mm	
Desired Rotation	0.00380		radians	
Available Rotation in Radius due to Compression of Pad	0.02215		radians	**OK**
Diameter / Thickness Ratio	13.54	Maximum (Dpad/he)	15	**OK**

Check for Min. average Stress (Clause - 5.2.3.3)

Min. average stress = (Nsd min. / a)	8.11	N/mm²		
Permissible Min. average stress =	2.00	N/mm²		
	OK			

Design Calculation of SLS- 1647 KN, ULS- 2365 KN Longitudinal Guided Bearing

Pressure on PTFE

Diameter of PTFE		L	325.00		mm
Area of PTFE		Aco	82957.68		mm²
Average pressure on PTFE =	Nmax ULS / Ap	σ p	28.51		N/mm²
Protrusion of PTFE					
h = 1.75 + L / 1200			2.02		mm
h provided			2.20		mm
Thickness of PTFE = 2.2h			4.84		mm
Thickness of PTFE provided			5.00		mm
			OK		
Characteristic compressive strength of PTFE		fk	90.00		N/mm²
The Characteristic compressive strength is reduced due to exceeding the category temperature above 30°C.					
Max. ambient temperate			**43.00**		°C
Reduction			26.00		%
Reduction factor		k	0.74		
μ max = 1.2 / (10 + σ p)			0.031		
	0.03	≤	0.031	≤	0.08
e1 = μ max x R			5.06		mm
e3 = αd x L/2			0.62		mm
e = e1 + e3			5.68		mm
		L/8	40.63		mm
			OK		
λ = (1 − 0.75 x π x e / L)		λ	0.96		
Reduced contact area	Ar = Aco x λ	Ar	79540.77		mm²
max,Nsd = Ar x k x fk / γm	γm = 1.4		3783.87		kN
Nsd, ULS			2365.00		kN
			OK		

Stress in bottom concrete

Bottom dispersion width				**Do**	**395**
Thickness of Bottom Plate				**kb**	**20**
Area of Bottom Dispersion= p x d ^ 2/4		a		122591.071	mm²
Section Modulus = p x d ^ 3/32		Z		6052934.152	mm³
Vertical Load		Nsd	2365.00		kN
Horizontal force		Vsd	0.00		kN
Moment of resistance due to rotation:					
Rotation due to dead load		θ p	0.00155		radians
Live Load		θ v	0.00225		radians
Ratio = di / he			13.54		
For induced moment		k1	1.97		
		k2	76.38		
Induced moment due to rotation Me.d					
di³ x (k1x qp+K2 x qv)/1000		Me.d	5997.30		kN-mm
Moment of resistance due to HF:					
Horizontal distance		C	162.50		mm
Resultant HF		Vsd	0.00		kN
Moment of resistance due to HF:		Mr.d	0.00		kN-mm
0.2 x C x Vsd					
Total Movement = Me.d+Mr.d =		Mt	5997.30		kN-mm
Direct Pressure Nsd / a		pa	19.29		N/mm²
Permissible Stress (0.67 x fck) / 1.5		fcd	20.10		N/mm²
			OK		
Bending Stress Mt / Z		pb	0.99		N/mm²
Permissible bending stress			14.85		N/mm²
			OK		
Area on Pedestal		Ac1	490167.00		mm²
Frdu= Aco x fcd x (sqrt(Ac1 / Ac0)			4926.18		kN
3 x fcd x Aco			7389.27		kN
Frdu </= 3 x fcd x Aco			**OK**		

Design Calculation of SLS- 1647 KN, ULS- 2365 KN Longitudinal Guided Bearing

Stress in top concrete

Top dispersion width				**Dtpeff**	**375**
Thickness of Top Plate				**Tt**	**22**
Area of Top Dispersion = p x d ^ 2/4	a			110491.071	mm²
Section Modulus = p x d ^ 3/32	Z			5179268.973	mm³
Vertical Load	Nsd		2365.00		kN
Horizontal force	Vsd		0.00		kN
Moment of resistance due to rotation:					
Rotation due to dead load	θ p		0.00155		radians
Live Load	θ v		0.00225		radians
Ratio = di / he			13.54		
For induced moment	k1		1.97		
	k2		76.38		
Induced moment due to rotation	Me.d				
di³ x (k1x qp+K2 x qv)/1000			5997.30		kN-mm
Moment of resistance due to HF:					
Horizontal distance	C		162.50		mm
Resultant HF	Vsd		0.00		kN
Moment of resistance due to HF:	Mr.d		0.00		kN-mm
0.2 x C x Vsd					
Total Movement = Me.d+Mr.d =	Mt		5997.30		kN-mm
Direct Pressure Nsd / a	pa		21.40		N/mm²
Permissible Stress (0.67 x fck) / 1.5	fcd		22.33		N/mm²
			OK		
Bending Stress Mt / Z	pb		1.16		N/mm²
Permissible bending stress			16.50		N/mm²
			OK		
Area on Superstructure	Ac1		441786.47		mm²
Frdu= Aco x fcd x (sqrt(Ac1 / Ac0)			4933.28		kN
3 x fcd x Aco			7399.92		kN
Frdu </= 3 x fcd x Aco			**OK**		

Pot walls subjected to tensile force (Clause 5.3.1.2.3)

AR = (do - di) x hc	AR	1800.00		mm²
Ve,sd = 4 x Nsd x he / π x di	Ve,sd	222.48		kN
Vfxy,sd		0.00		kN
Vsd = Ve,sd + Vfxy,sd		222.48		kN
Vrd = fy x AR / Ym Ym =	1.1	556.36		kN
		OK		

Pot walls subjected to shear force (Clause 5.3.1.2.4)

V'sd ≤ V'Rd				
V'sd = Ve,sd + 1.5 x Vfxy,sd /di		0.68		kN
V'Rd = (fy x (do - di)) / (2 x Ym x (sqrt(3)))	Ym = 1.1	5.15		kN
		OK		

Pot base subjected to tensile force (Clause 5.3.1.2.5)

Vsd ≤ VRd				
Ap = do x kb		7500.00		mm²
Vsd = Ve,sd + Vfxy,sd		222.48		kN
VRd = fy x Ap / Ym Ym =	1.1	2318.18		kN
		OK		

Design resistance for integral guides

Shear resistance

Thickness of guide	ku	15.00	mm	
Height of guide	Hgb	18.00	mm	
Length of guide	Lgb	420.00	mm	
Length of side sliding	L	365.00	mm	
Height of application	ha	10.50	mm	
Effective length of guide	Leff	386.00	mm	
Vsd ≤ VRd Ym =	1.1			
VRd = ku x Leff x fy / √3 x Ym		1033.25	kN	
Vsd		0.00	kN	
		OK		

Design Calculation of SLS- 1647 KN, ULS- 2365 KN Longitudinal Guided Bearing

Bending resistance in combination with shear resistance

P = ((2 x Vsd / V_{Rd}) - 1)^2	1.00		
f'y = (1 - P) x fy	0.00		
M_{Rd} = ku^2 x Leff x f'y / (4xYm)	0.00	kN-mm	
Msd = Vsd x ha	0.00	kN-mm	
	OK		

Movement Capacity

Size of Top Plate	Lt	=	420.00	mm
	Bt	=	410.00	mm
Effective contact Concrete Diameter	Dtpeff	=	375.00	mm
Preset (If Any)		=	0.00	mm
Long. Movement Capacity (Lt - Dtpeff)		=	45.00	mm
Movement in One Direction		=	22.50	mm
Permissible Movement		=	21.00	mm
			OK	
Movement in Other Direction		=	22.50	mm
Permissible Movement		=	21.00	mm
			OK	

Anchor Bolts

Max Horzontal Force			0.00	kN
Min. Vertical Load			**1150.00**	kN
Frictional Force			**0.00**	kN
Diameter of Bolt			**16.00**	mm
Length of Bolt			**35.00**	mm
Number of Bolts	**n**		**4.00**	Nos.
Thickness of Collar	Ct		12.00	mm
Factor for Net Area	kn		0.78	
Effec. Area of Bolt (p x $d274^2$ x kn / 4)	Abolt		156.89	mm^2
αv			0.60	
fub			800.00	N/mm^2
Ym^2			1.25	
fu			570.00	N/mm^2
k2			0.90	
Shear resistance $F_{v,Rd} = \alpha v \times fub \times A / Ym^2$		$F_{v,Rd}$	60.25	kN
Resultant horizontal force / bolt Vfxy,sd / n		$F_{v,sd}$	0.00	kN
			OK	
Bearing resistance $F_{b,Rd} = 1.25 \times fu \times d \times t / Ym^2$		$F_{b,Rd}$	109.44	kN
Resultant horizontal force / bolt Vfxy,sd / n			0.00	kN
			OK	
Tension resistance $F_{t,Rd} = k2 \times fub \times As / Ym^2$		$F_{t,Rd}$	90.37	kN
Design tension resistance		$F_{t,sd}$	0.00	kN
Combined shear and tension=Fv,sd / $F_{v,Rd}$ + Ft,sd / (1.4 x $F_{t,Rd}$)			0.00	
			OK	

Anchor Sleeves (Clause - 5.3.6.4.2)

Top Plate		
Length of Sleeve	**110.00**	mm
Diameter of Sleeve	**40.00**	mm
Number of Sleeves	4.00	Nos.
Resistance offered by concrete F_{Rdu} = 1.33 D x L x fcd / sqrt(3)	75.46	kN
Design resistance in shear	0.00	kN
	OK	
Bottom Plate		
Length of Sleeve	120.00	mm
Diameter of Sleeve	**40.00**	mm
Number of Sleeves	4.00	Nos
Resistance offered by concrete F_{Rdu} = 1.33 D x L x fcd / sqrt(3)	74.08	kN
Design resistance in shear	0.00	kN
	OK	

Design Calculation of SLS- 1647 KN, ULS- 2365 KN Longitudinal Guided Bearing

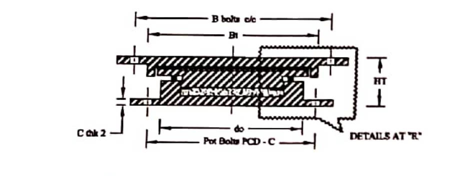
Requirement of clearance

$\delta = 0.01 \times Di$	min. = 3		3.25	<	10	mm
hc - he - (w - we) x 0.5 - (Θ x 0.5 x Di)			8.38			mm
δ			**3.25**			mm
			OK			
hp - (hc - he) - (Θ x 0.5 x Dp)			**9.31**			mm
δ			**3.25**			mm
			OK			

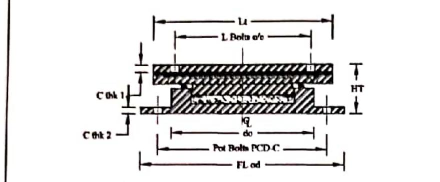
Curved Contact Surface (Clause - 5.3.1.4.2)

Vsd ≤ Vrd	R	=	162.50	mm
	fu	=	570.00	N/mm²
	θ	=	0.004	Radian
	Ym	=	1.10	
Vrd = 15 x fu^2 x R x Di / Es x Ym^2		=	1063.6	kN
Vsd		=	0.00	kN
			OK	
we = 3.04 x (sqrt(1.5 x Vsd x R / Es x Di)		=	**0.00**	mm
we + Θ x Di		=	**1.24**	mm
Provided	w	=	6.00	mm
			OK	

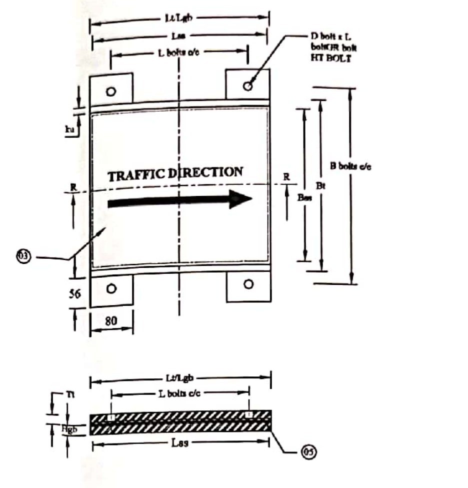
KARMA ENTERPRISE Guwahati



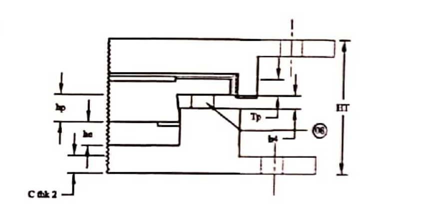
SECTIONAL TRANSVERSE ELEVATION OF BEARING ASSEMBLY



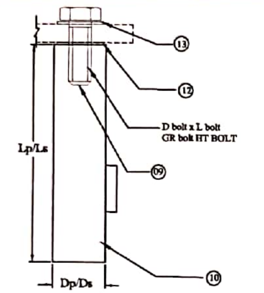
SECTIONAL LONGITUDINAL ELEVATION OF BEARING ASSEMBLY AT "R-R"



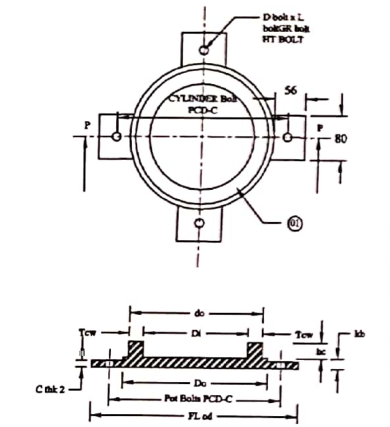
SECTIONAL ELEVATION OF TOP PLATE AT "R-R"



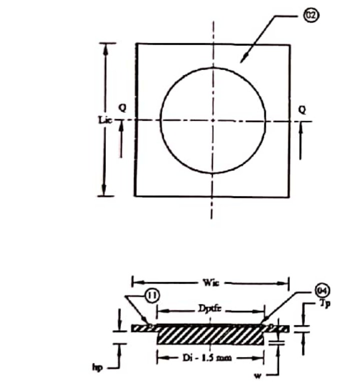
DETAILS OF BEARING ASSEMBLY AT "R"



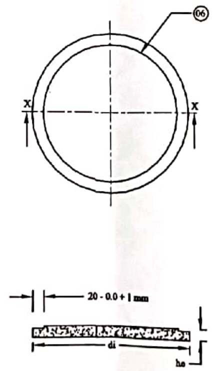
DETAILS OF ANCHORAGE



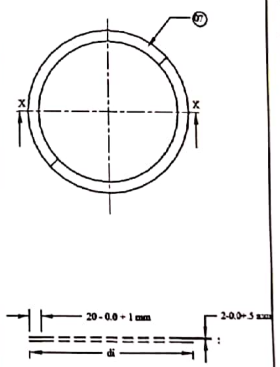
SECTIONAL ELEVATION OF BOTTOM CYLINDER AT "P-P"



SECTIONAL ELEVATION OF INTERMEDIATE COMPONENT AT "Q-Q"



PLAN OF PAD (TOP VIEW)



PLAN OF BRASS RING (TOP VIEW)

S. NO.	DESCRIPTION	MATERIAL	QTY	SPECIFICATION
13.	FLAT WASHER	STEEL	08	STD
12.	NEOPRENE WASHER		08	ELASTOMER
11.	WIPER SEAL	NEOPRENE	1	ELASTOMER
10.	DOWELS	MILD STEEL	08	IS : 2062 / IS : 226
9.	BOLT M16	Gr. 8.8 HT	08	IS : 1367
8.	DUST SEAL	FLEXIBLE FOAM	1	BITUMEN IMPRIGNATED
7.	BRASS RING	BRASS	2	HALF HARD BRASS
6.	NEOPRENE PAD	NEOPRENE	1	IRC : 83 (PART III)
5.	STAINLESS STEEL PLATE x 3mm		1	AISI : 316 L
4.	DIMPLED PTFE	PTFE BS-5400	1	Gr. A of BS : 3784
3.	SLIDE PLATE	MILD STEEL	1	IS : 2062
2.	PISTON	CAST STEEL	1	IS : 1030 Gr. 340 - 570 W
1.	POT	CAST STEEL	1	IS : 1030 Gr. 340 - 570 W

Bearing Type	Case	Vertical Load (KN) Max.	Vertical Load (KN) Min.	Hor. Load (KN) Long.	Hor. Load (KN) Trans.	Movement L : T (mm)
Longitudinal Guided Bearing	SLS	1643.0	673.0	0.00	0.00	+21.0 / -21.0 : ±0.0
	ULS	2365.0	1150.0	0.00	0.00	

NOTES

MATERIALS :
1. CONFINED ELASTOMER INSIDE POT WILL HAVE FOLLOWING PROPERTIES
 a) HARDNESS IRHD IS:3400 (PART II) 50±5
 b) MIN. TENSILE STRENGTH MPa IS:3400 (PART I) 15.5
 c) MIN ELONGATION AT BREAK , MAX COMPRESSION SET & ACCELERATED AGING WILL BE AS PER TABLE -1 - PROPERTIES OF ELASTOMER IN IRC:83(PART II)
2. ANCHORES: HT BOLTS OF Gr. 8.8 & SLEEVE MATERIAL AS PER IS 2062.
3. ACCESSORIES TO IS 226 / 2062.
4. CONFINED PTFE WILL BE OF UNFILLED QUALITY AND WILL HAVE REQUIRED PROPERTIES REGARDING TENSILE STRENGTH ETC. AS PER BS:5400 SEC 9.2 , BS 3784 & BS 6564 THE THICKNESS SHALL BE > OR = 4.5 MM.
5. THE STAINLESS STEEL STEEL SHALL BE STICH WELDED / SCREWED ON THE BACKING PLATE.
6. **CONCRETE GRADE FOR PEDESTAL IS M45.**
7. **CONCRETE GRADE FOR SUPERSTRUCTURE IS M50.**
8. **PRESET IN LENGTH FROM THE CENTER = 00.00 mm**

WELDING :
ALL WELDING WILL BE MANUAL METAL ARC PROCESS CONFORMING TO IS: 814,PRE HEATING & POST WELD STRESS RELIEVING TO BE DONE IF REQUIRED.

FINISHING :
a) ALL NONWORKING SURFACES WILL BE COATED WITH 2 COATS OF EPOXY PRIMER & ONE OR MORE COATS EACH OF EPOXY INTERMEDIATE AND FINISH PAINT. TOTAL DRY FILM THICKNESS > 160 MICRONS.
b) ANCHORE SLEEVES WILL BE CEMENT COATED AT SITE (IF REQUIRED).

GREASING :
SILICON GREASE WILL BE APPLIED AT PTFE STAINLESS STEEL INTER FACE.

TESTS :
a) TESTS ON CASTING: TESTS SPECIFIED IN IS : 1030 WILL BE PERFORMED. CASTINGS SHALL BE ULTRASONICALLY TESTED & CERTIFICATES SUBMITTED. QUALITY LEVEL 3 AS PER IS : 9565.

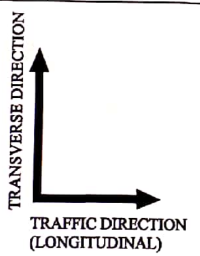
b) ACCPETANCE TEST ON BEARINGS.

c) ALL TESTS ON BEARINGS WILL BE CARRIED OUT IN PRESENCE OF REPRESENTATIVE OF DPT./ P.M.C. NECESSARY TEST CERTIFICATES FOR RAW MATERIALS SHALL BE FURNISHED AT THE TIME OF SUPPLY.

d) TEST ON WELDING: WELDING WILL BE TESTED BY DYE PENETRATION METHOD. BUTT WELDING WILL BE TESTED BY ULTRASONIC METHOD SOUNDNESS OF WELDING SHALL BE CERTIFIED BY THE MANUFACTURER

CAPACITY	Do	kb	Di	do	hc	Tcw	PCD	FL od	Cthk 2	Lt	Bt	Tt	Lss	Bss	Tss	Lc/c	Bc/c	Cthk 1	Lgb	ku	Hgb	Lic	Wic	Tp	hp	w	Dptfe	Tptfe	di	he	Dp	Lp	Ds	Ls	Dbolt	Lbolt	Nbolt	GRbolt	h4	HT
2365 KN- LG	395	20	325	375	36	25	443	507	12	420	410	22	410	370	03	340	458	12	420	15	18	365	365	12	22	06	325	5	325	24	40	120	40	110	16	35	04/04	8.8	10	105.2
	DIMENSION DETAIL OF CYLINDER									DIMENSION DETAIL OF TOP PLATE									GUIDE BAR			INTERMEDIATE COMPONENT DIM.							PAD		ANCHORAGE & SLEEVE									

1) ALL DIMENSIONS ARE IN mm UNLESS OTHERWISE MENTIONED.
2) PCD = PITCH CIRCLE DIAMETER
3) TOLERANCES
 a) PLAN DIMENSIONS : -0 TO +5mm
 b) OVERALL HEIGHT : -0 TO +3mm
 c) HEIGHT OF ELASTOMER : -0 / + 5%
 d) HEIGHT OF ANY STEEL COMPONENT
  1) MACHINED : -0 TO +1mm
  2) UNMACHINED : CLASS 2 OF IS :4897

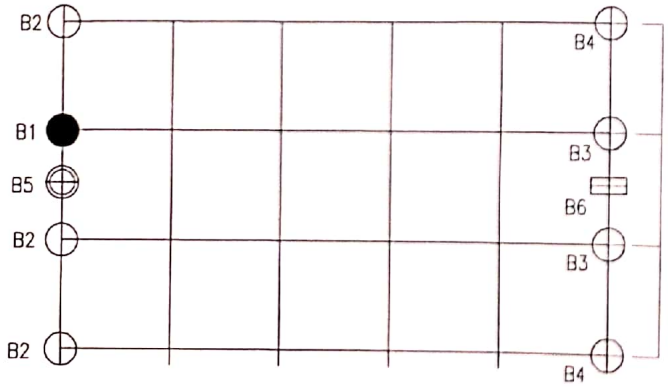


TYPE :- LONGITUDINAL GUIDED BEARING
TYPE :- B3
CH. :- 516+938

KARMA ENTERPRISE * Guwahati *

Project	Four Laning of Jhanjhi to Demow Section from KM. 491+050 to 535+250 (Design KM. 490+800 to KM. 534+800) of NH-37 in the State of Assam under SARDP on Engineering Procurement & Construction (EPC) mode	Manufacturer & Supplier :- KARMA ENTERPRISE, GUWAHATI
Client	NHIDCL	
Authority Engineer	M/s Voyants Solutions Pvt. Ltd.	
Contractor	M/s Kamac Engineers Pvt. Ltd., M/s Shiva Harlalka (JV)	
Title	GAD of SLS-1647 KN, ULS-2365 KN Longitudinal Guided Bearing	

BEARING TYPE & LOAD DETAILS				FIXED BEARING	LONG FIXED BEARING	TRANS FIXED BEARING	FREE BEARING	PIN BEARING	MEATALIC GUIDED BEARING
BEARING MARK				B1	B2	B3	B4	B5	B6
TOTAL QUANTITY (NO)				1	3	1	3	1	1
GRADE OF CONCRETE	UPPER SURFACE	SLS		M50	M50	M50	M50	M50	M50
		ULS		M50	M50	M50	M50	M50	M50
	LOWER SURFACE	SLS		M45	M45	M45	M45	M45	M45
		ULS		M45	M45	M45	M45	M45	M45
DESIGN LOAD (KN)	SLS	VERTICAL	MAX	1647	1647	1647	1647	-	-
			PERMENANT	843	843	843	843	-	-
			MIN	673	673	673	673	-	-
		LONGITUDINAL		50	50	0	0	-	-
		TRANSVERSE		0	0	0	0	-	-
	ULS	VERTICAL	MAX	2365	2365	2365	2365	-	-
			PERMENANT	1150	1150	1150	1150	-	-
			MIN	1	1	1	1	-	-
		LONGITUDINAL		75	75	0	0	5548	0
		TRANSVERSE		0	0	0	0	2755	2755
TRANSLATION (MM)	SLS	IRREVERSABLE	LONG	-	-	-	-	-	-
			TRAN	-	-	-	-	-	-
		REVERSABLE	LONG	-	-	14	14	-	-
			TRAN	-	13	-	13	-	-
	ULS	IRREVERSABLE	LONG	-	-	-	-	-	-
			TRAN	-	-	-	-	-	-
		REVERSABLE	LONG	-	-	21	21	-	21
			TRAN	-	20	-	20	-	-
ROTATION (RED)	SLS	IRREVERSABLE	LONG	0.00253	0.00253	0.00253	0.00253	-	-
			TRAN	-	-	-	-	-	-
		REVERSABLE	LONG	0.00253	0.00253	0.00253	0.00253	-	-
			TRAN	-	-	-	-	-	-
	ULS	IRREVERSABLE	LONG	0.00380	0.00380	0.00380	0.00380	0.00380	0.00380
			TRAN	-	-	-	-	-	-
		REVERSABLE	LONG	0.00380	0.00380	0.00380	0.00380	0.00380	0.00380
			TRAN	-	-	-	-	-	-



KEY PLAN SHOWING ARRANGEMENT OF BEARING LOCATIONS FOR POT cum PTFE BEARINGS

B1 FIXED BEARING
B2 TRANS GUIDED BEARING
B3 LONG GUIDED BEARING
B4 FREE BEARING
B5 PIN BEARING
B6 METALLIC GUIDED BEARING

NOTES:

1. ALL DIMENSIONS ARE IN MILLIMETRES, LEVELS ARE IN METRES AND UNLESS OTHERWISE SPECIFIED, ONLY WRITTEN DIMENSIONS SHALL BE FOLLOWED.
2. THE CONTRACTOR SHALL SUBMIT DESIGN/ DRAWING OF INDIVIDUAL BEARINGS BASED ON LOAD DATA AS GIVEN IN THIS DRAWING FOR APPROVAL OF THE ENGINEER.
3. BEARINGS SHALL BE PROCURED FROM THE LIST OF APPROVED MANUFACTURER BY MORTH.
4. ALL BEARINGS SHALL CONFORM TO THE LATEST MORTH SPECIFICATION, IRC:83 (PART III)-2018 AND TENDER STIPULATION, IF ANY.
5. THE TESTING OF RAW MATERIALS, METALIC COMPONENTS, ELASTOMER & PTFE AND ACCEPTANCE TESTS ON BEARINGS SHALL CONFORM TO MOST SPECIFICATION/TENDER SPECIFICATION.
6. MANUFACTURER SHALL SUBMIT THE CERTIFICATES FOR LOAD TESTING AND DIMENSIONS OF BEARING.
7. SUITABLE ERECTION CLAMPS FOR SAFE TRANSPORTATION AND HANDLING ALONG WITH TEMPLATE FOR ALIGNMENT SHALL BE PROVIDED BY THE MANUFACTURER.
8. THE PLAN SIZE AND HEIGHT OF PEDESTAL SHALL BE ADJUSTED TO SUIT THE FINALISED SIZE OF BEARINGS AT THE TIME OF EXECUTION.
9. THE GROUT/BEDDING MORTAR SHALL BE OF HIGH STRENGTH FREE FLOWING NON-SHRINK TYPE.

CLIENT: National Highways & Infrastructure Development Corporation Limited.

PROJECT: FOUR LANING OF JHANJHI TO DEMOW SECTION FROM KM. 481+480 TO 538+280 (DESIGN KM. 480+600 TO KM. 534+600) OF NH-67 IN THE STATE OF ASSAM UNDER BARDP ON ENGINEERING PROCUREMENT & CONSTRUCTION (EPC) MODE.

CONTRACTOR: M/S KAMAC ENGINEERS PVT.LTD M/S BHIVA HARILALKA (JV).

DESIGN DIRECTOR: Prateek Srivastava

PROOF CONSULTANT: TASPL

SAFETY CONSULTANT: VA INFRA ENGINEERING

AUTHORITY ENGINEER: VOYANTS SOLUTIONS PVT.LTD

SCALE: AS SHOWN

PREPARED	DESIGNED	CHECKED	APPROVED
K.R	G.R	P.S	P.S

DRG. NO. NHIDCL/KSUA/SUP/MNB/07-08

DATE : MAR. 2023 REVISION: R0

TITLE: BEARING LOAD DATA FOR MINOR BRIDGE AT KM-516+938